
Development of a Cohesive Zone Model for Adhesive Joints that Includes Humidity and Fatigue Degradation

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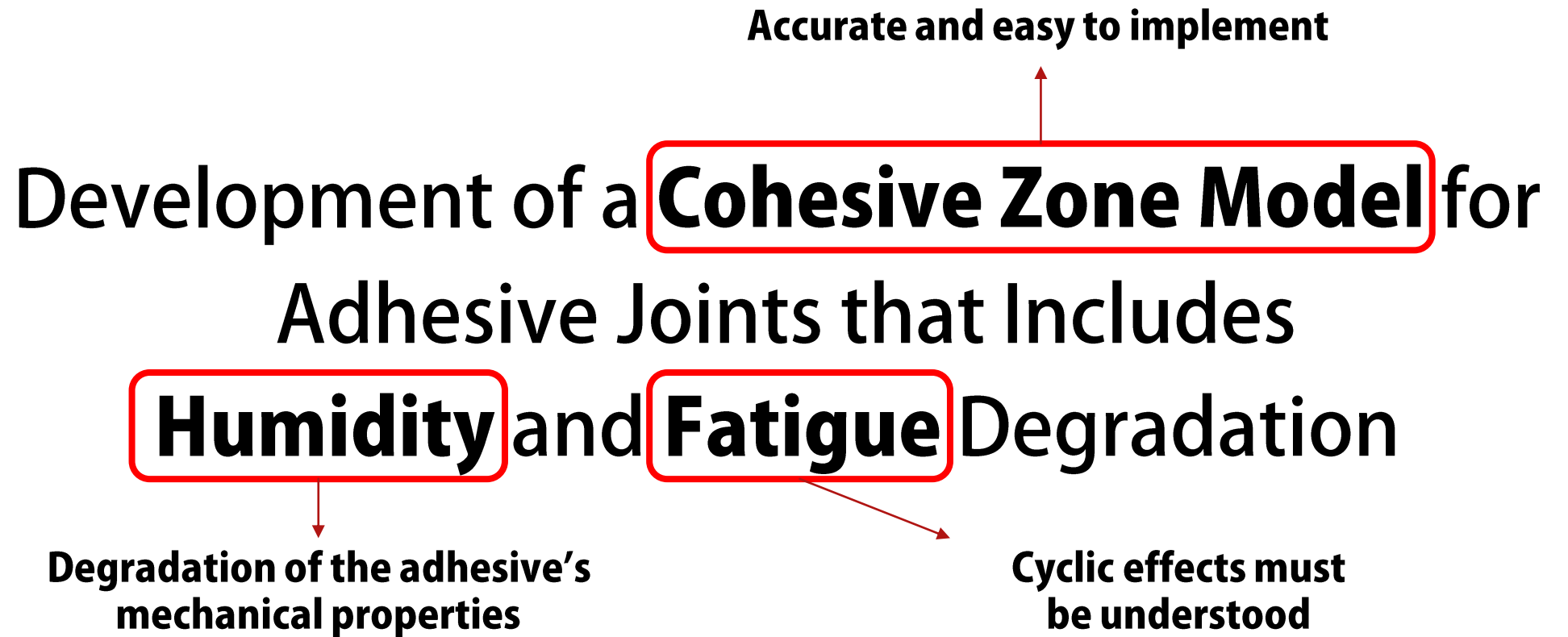
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Motivation



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Objectives

- Study the effects of humidity ageing in two different adhesives
 - Obtain Fick's law and diffusion coefficients
- Study the effect of fatigue of aged and unaged adhesives
 - Obtain Paris Laws for all situations
- Model those results numerically through the use of a custom Cohesive Zone Model
 - Development of an ABAQUS® user element routine

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Humidity

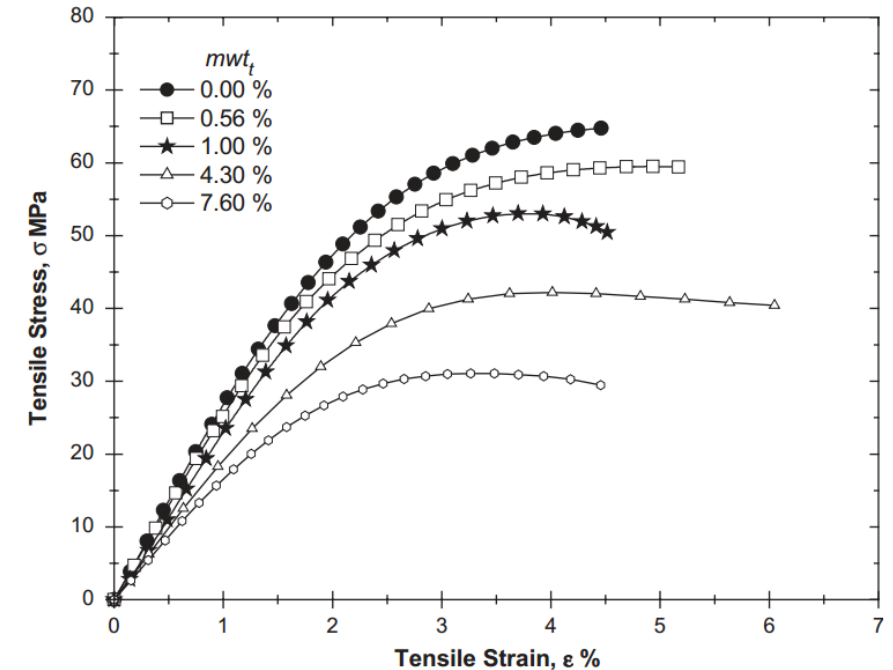
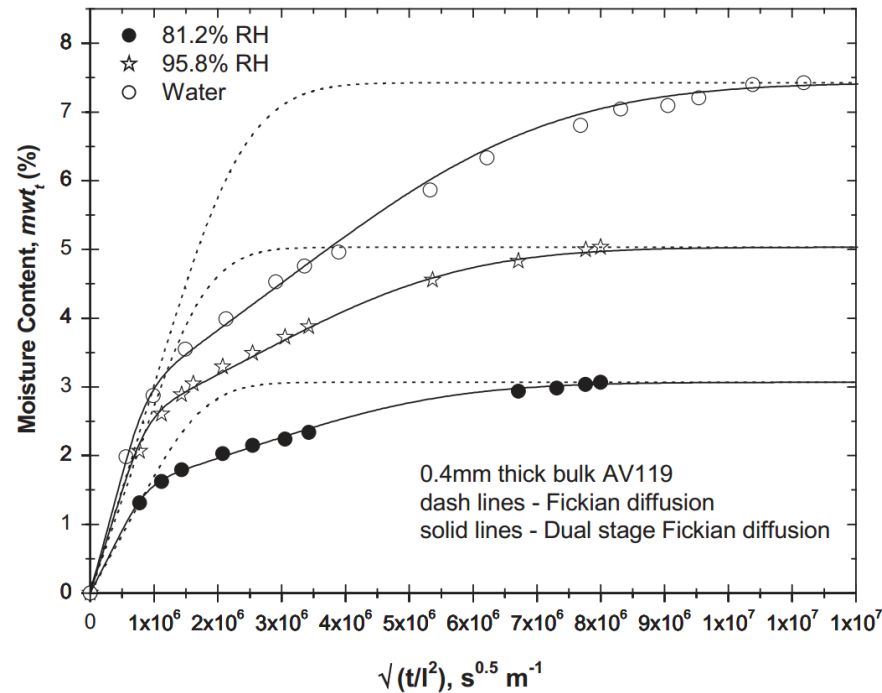


Fig. 1 – (left) Fickian diffusion plots, (right) Stress-strain curves for the same adhesive with different water concentrations. [W.K. Loh et al. (2005)]

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Humidity – Surface treatment

- Due to humidity, water can penetrate the interface between the adhesive and adherend – using a surface treatment improves the interface strength
- PAA (phosphoric acid anodizing) produces a very porous oxide coating, and highly adherent surface [G. Critchlow (2013)]

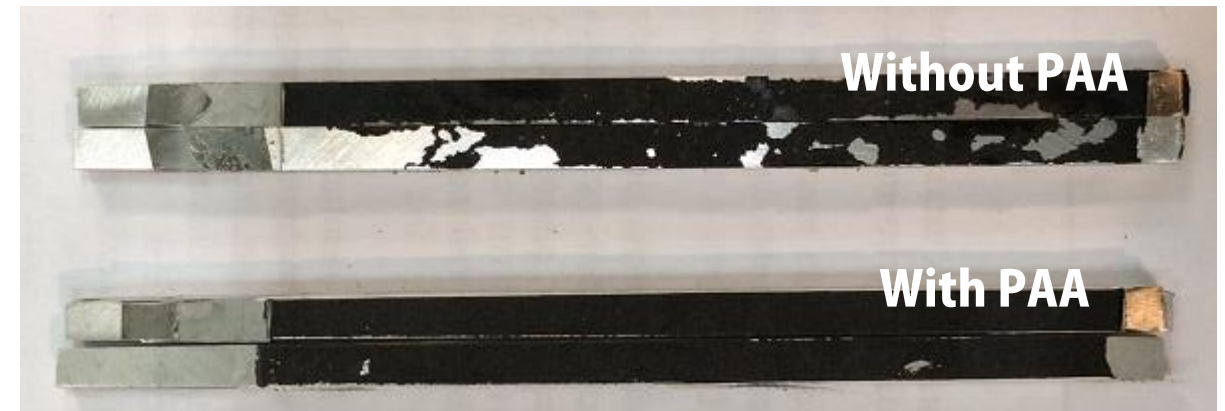
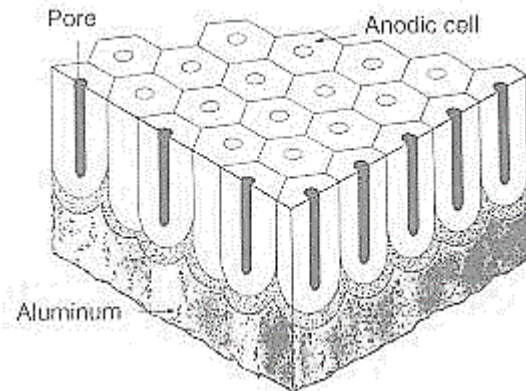


Fig. 2 – PAA microscopic structure (left), and differences in testes joints due to PAA (right).

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Humidity and fatigue combined

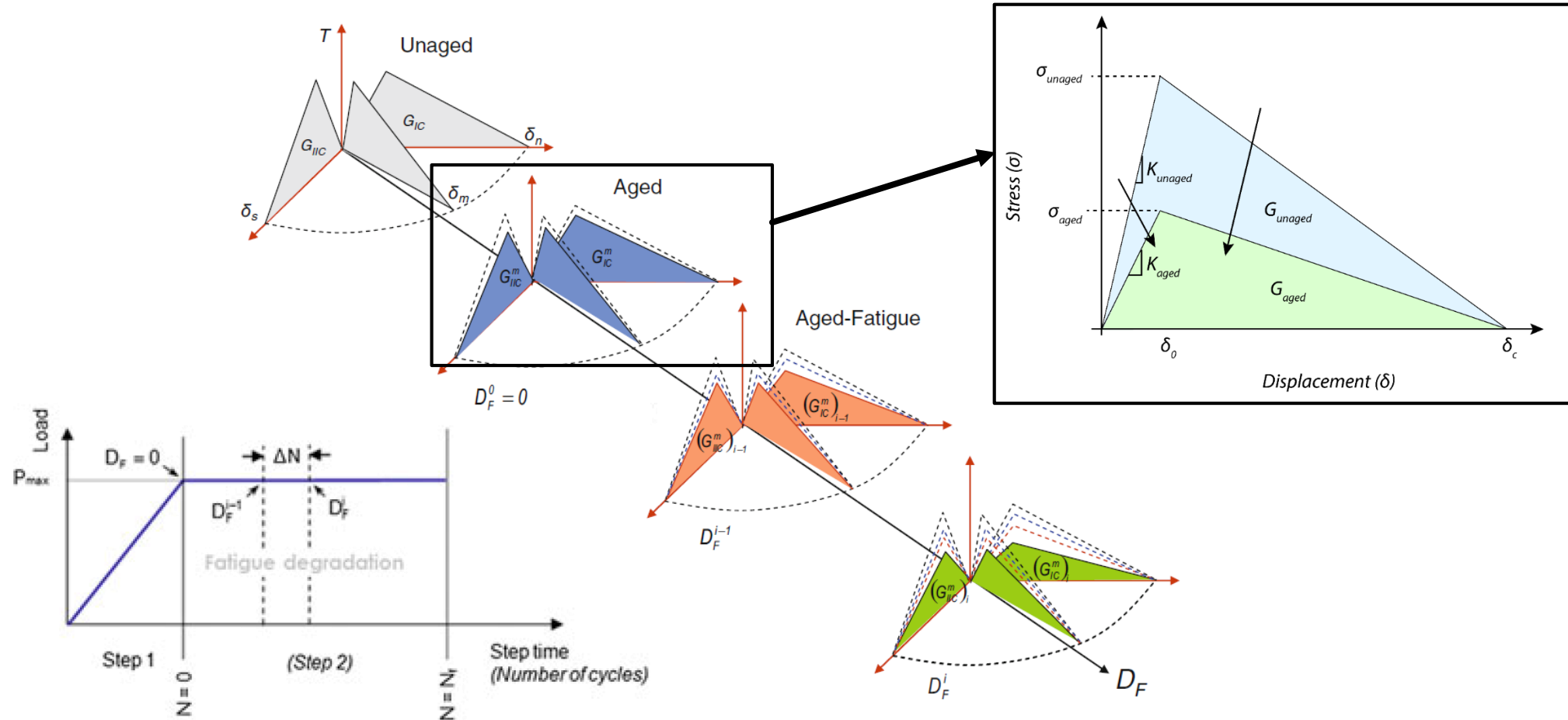


Fig. 3 – Degrading the CZM by both humidity and fatigue. [A.D. Crocombe et al. (2013)]

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Experimental procedure

- Optimised specimens were used (needed due to humidity tests).

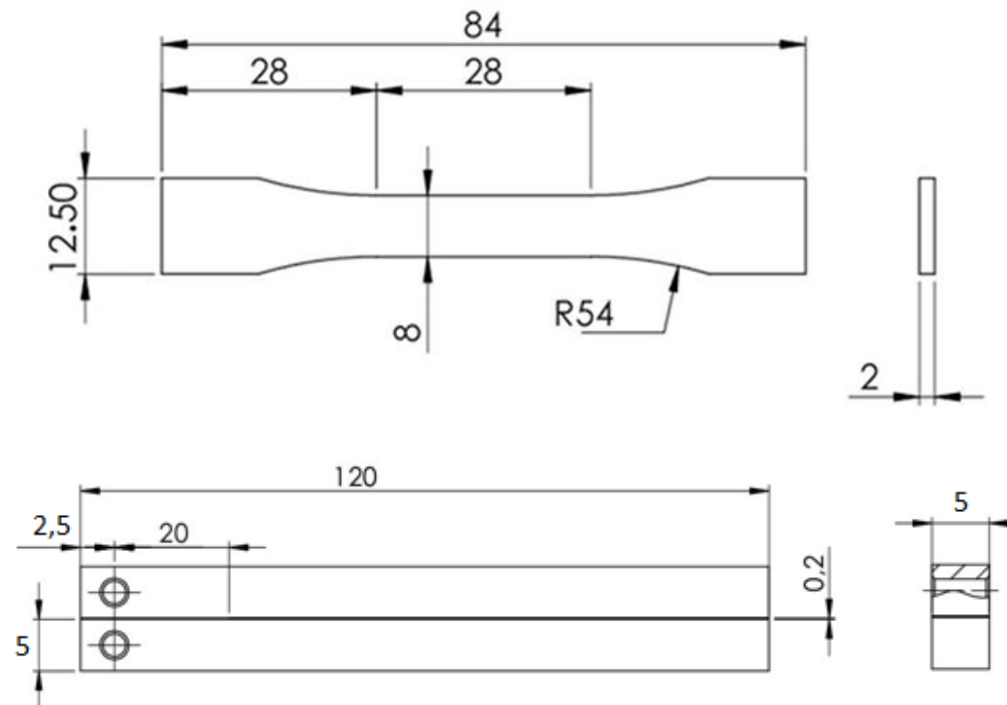


Fig. 4 – Optimised bulk specimens (top), optimised DCB specimens (bottom).

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Experimental tests – adhesives

Table 1 – Mechanical properties of both the adhesives used.

Adhesive	Tensile Strength (MPa)	Young's Modulus (MPa)	Strain to Failure (%)	G_{IC} (N/mm)
Nagase XNR 6852-1	56.4	2089.2	21.0	4.94
SikaPower 4720	25.0	2030	4.9	1.63

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Experimental tests – fatigue

- Step 1 – Static test to find maximum load

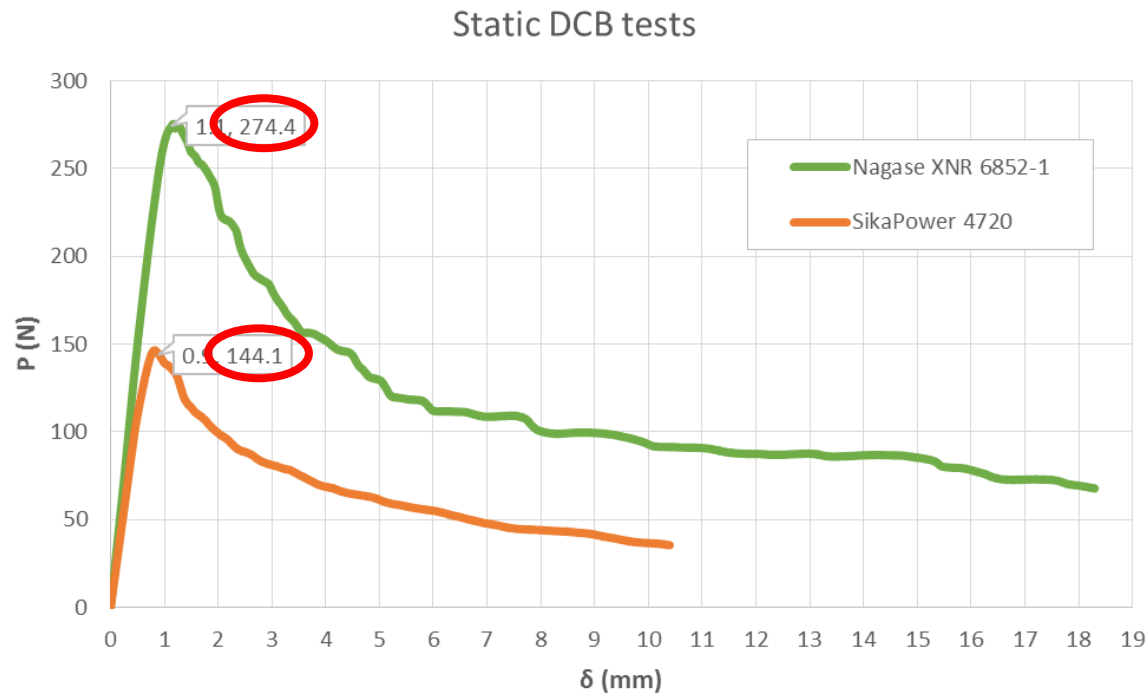


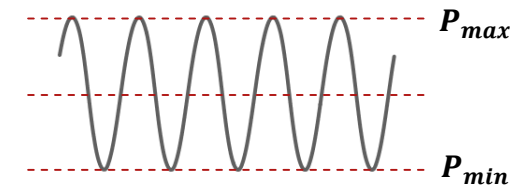
Fig. 4 – P- δ curves for both the tested adhesives, with the maximum load highlighted.

- Step 2 – Determine fatigue parameters

$$Fatigue \rightarrow \begin{cases} P_{max} = 60\% * P_{static} \\ P_{min} = 0.1 * P_{max} \end{cases}$$

Table 2 – Fatigue parameters.

Adhesive	P_{static} (N)	P_{max} (N)	P_{min} (N)
Nagase XNR 6852-1	274.4	165	16.5
SikaPower 4720	144.1	87	8.7



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Experimental tests – fatigue

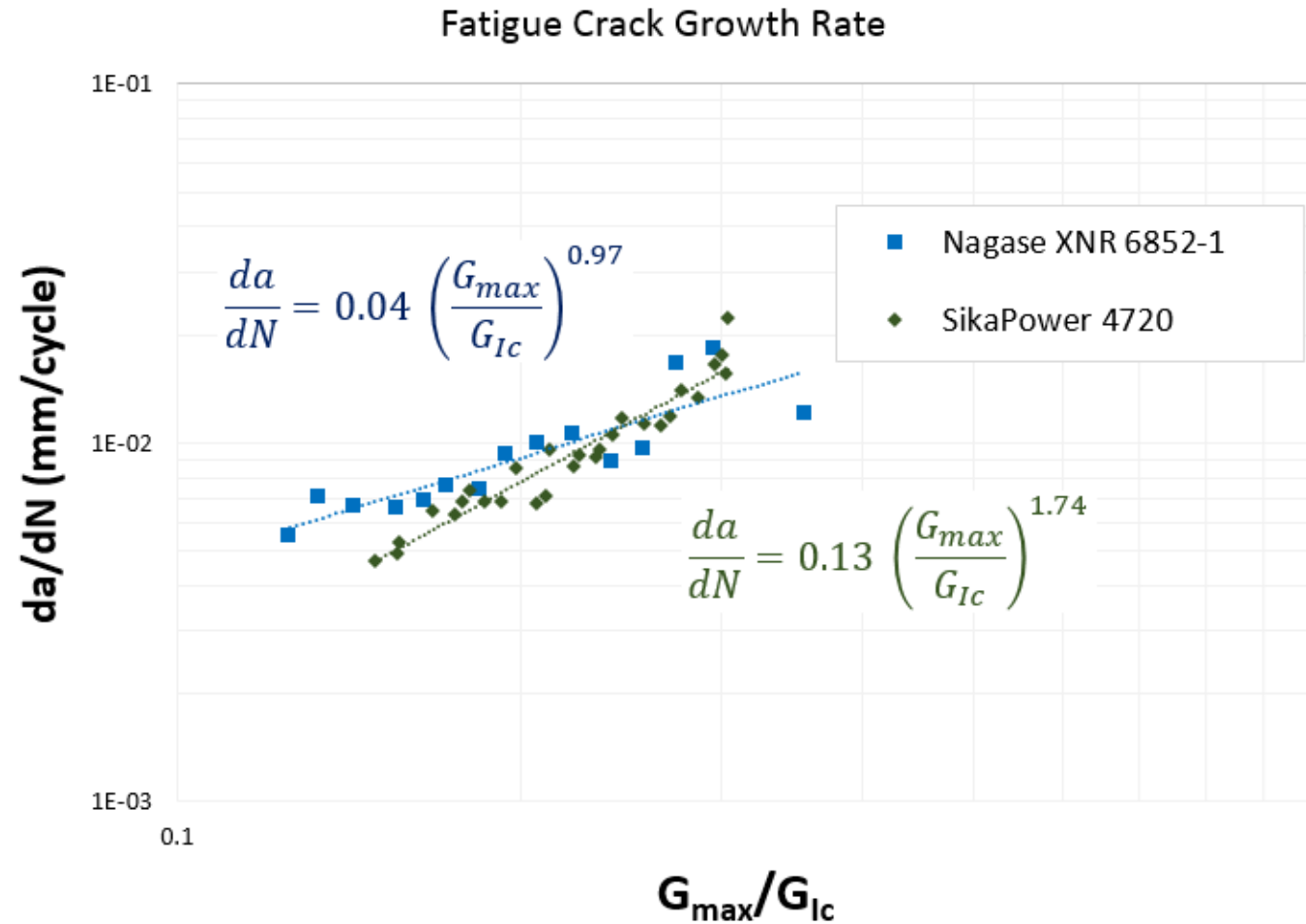


Fig. 5 – Paris Law curves and coefficients for both adhesives.

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Experimental tests – humidity

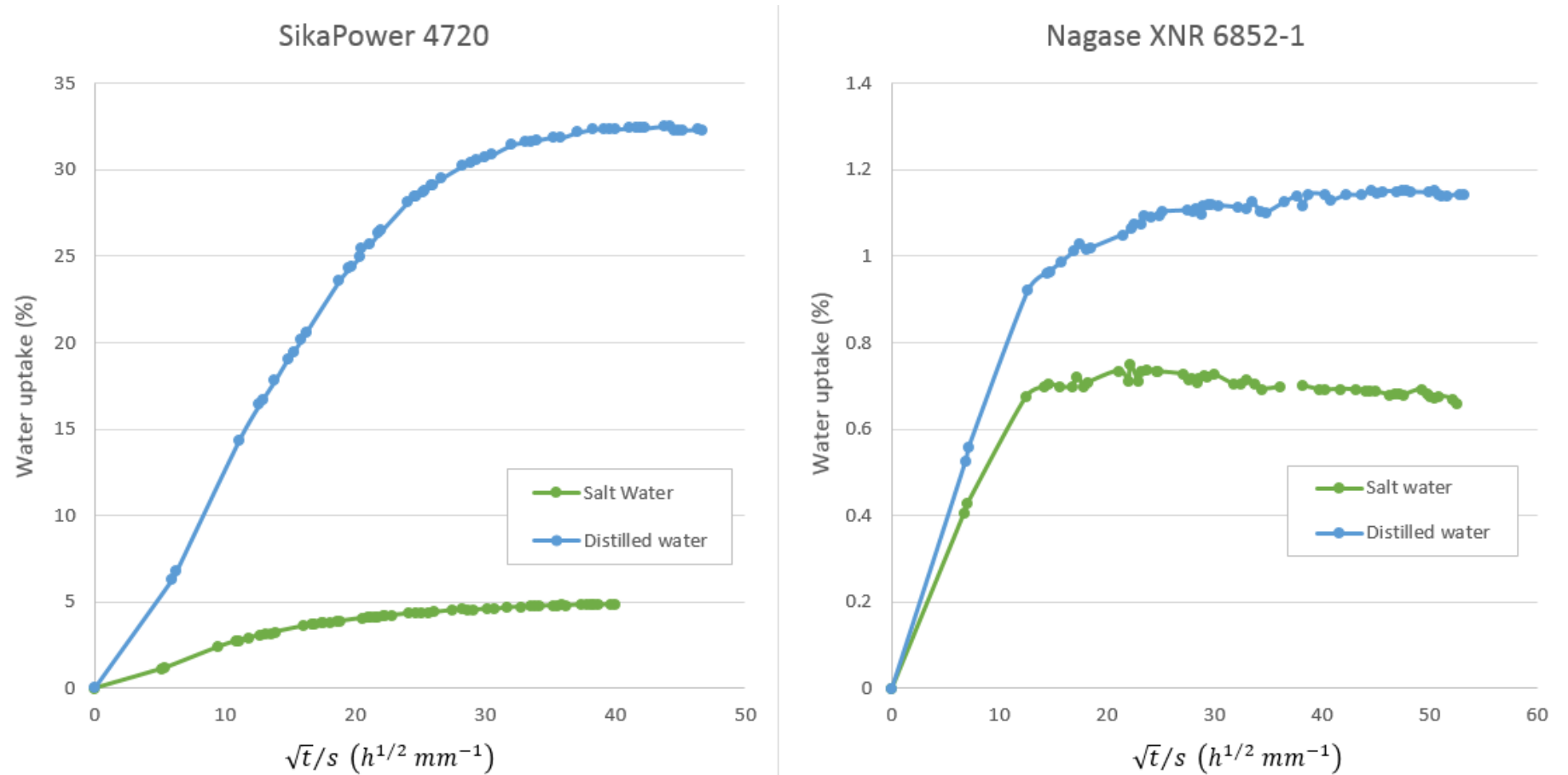


Fig. 6 – Diffusion plots for both tested adhesives.

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Numerical modelling

- Using ABAQUS® it is possible to develop custom finite element formulation (using FORTRAN®), called UEL routines
- Adopted approach: degrade the cohesive zone parameters in such a way that humidity and fatigue results can be obtained

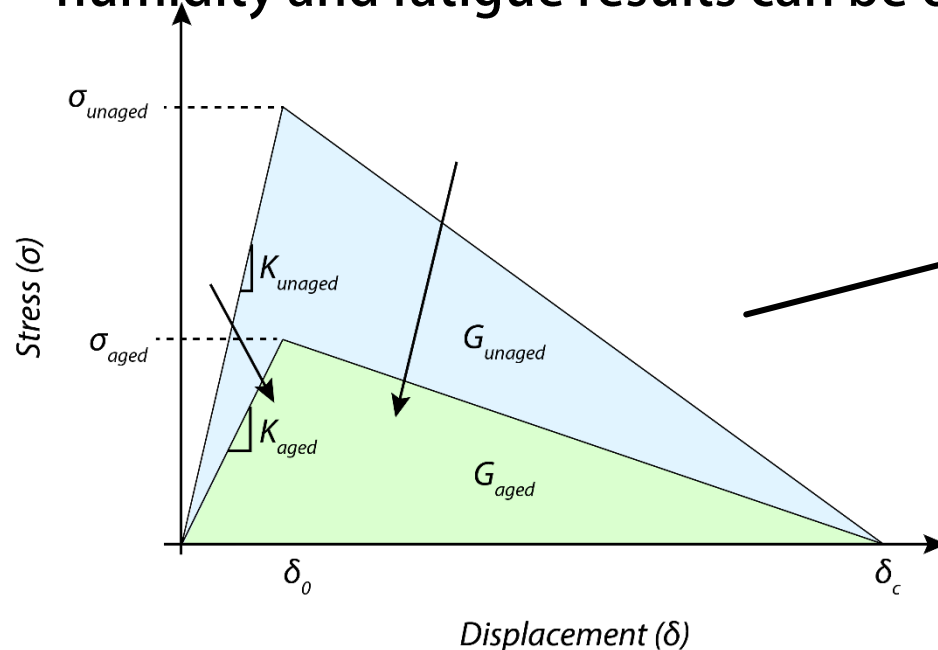


Fig. 7 – Cohesive zone model adapted to the humidity degradation.

$$\sigma_{aged} = \sigma_{unaged} * f_1(\text{humidity, Paris Law parameters, cycles, ...})$$
$$G_{aged} = G_{unaged} * f_2(\text{humidity, Paris Law parameters, cycles, ...})$$

More tests are needed to find out the exact relationships

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Numerical modelling

- UEL is created and working (with sample degrading coefficients):

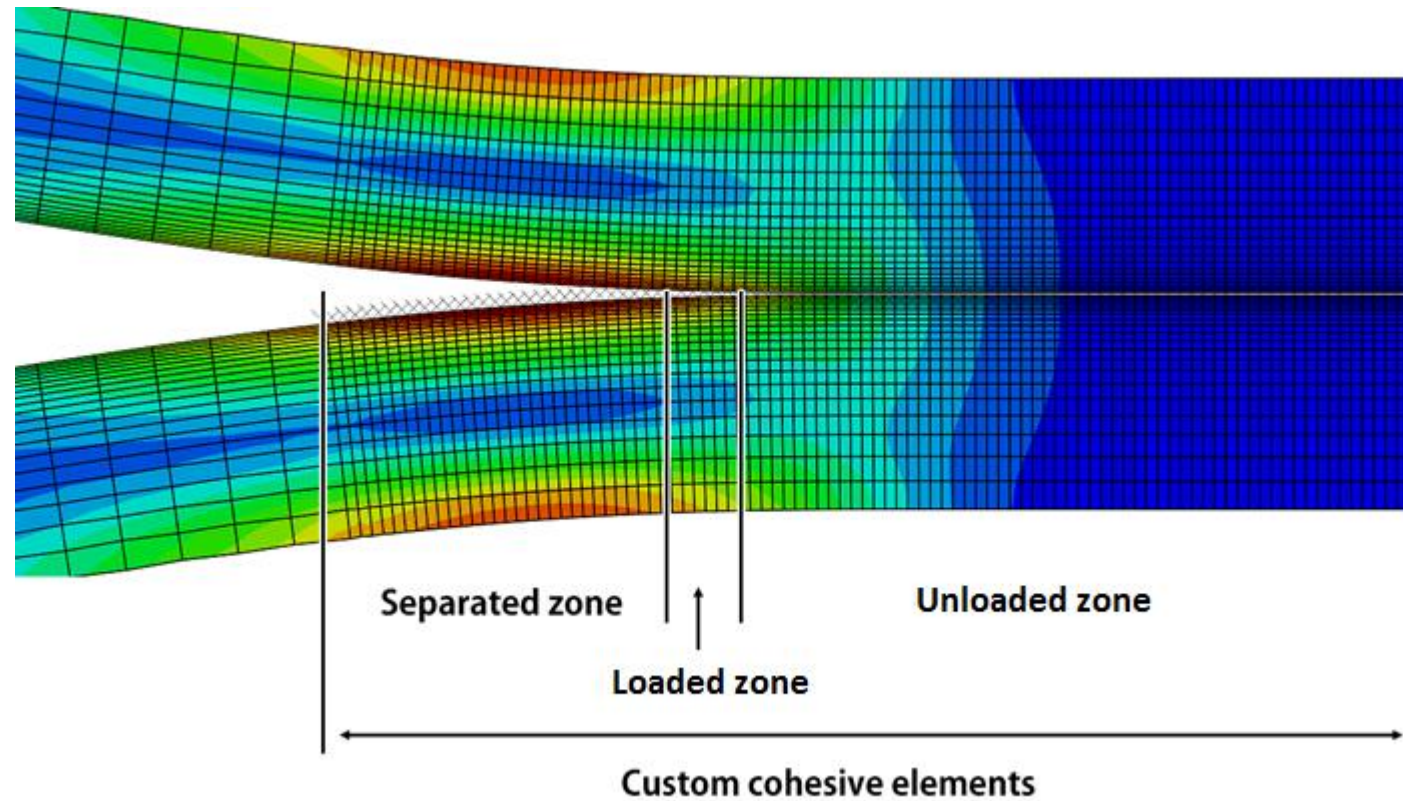


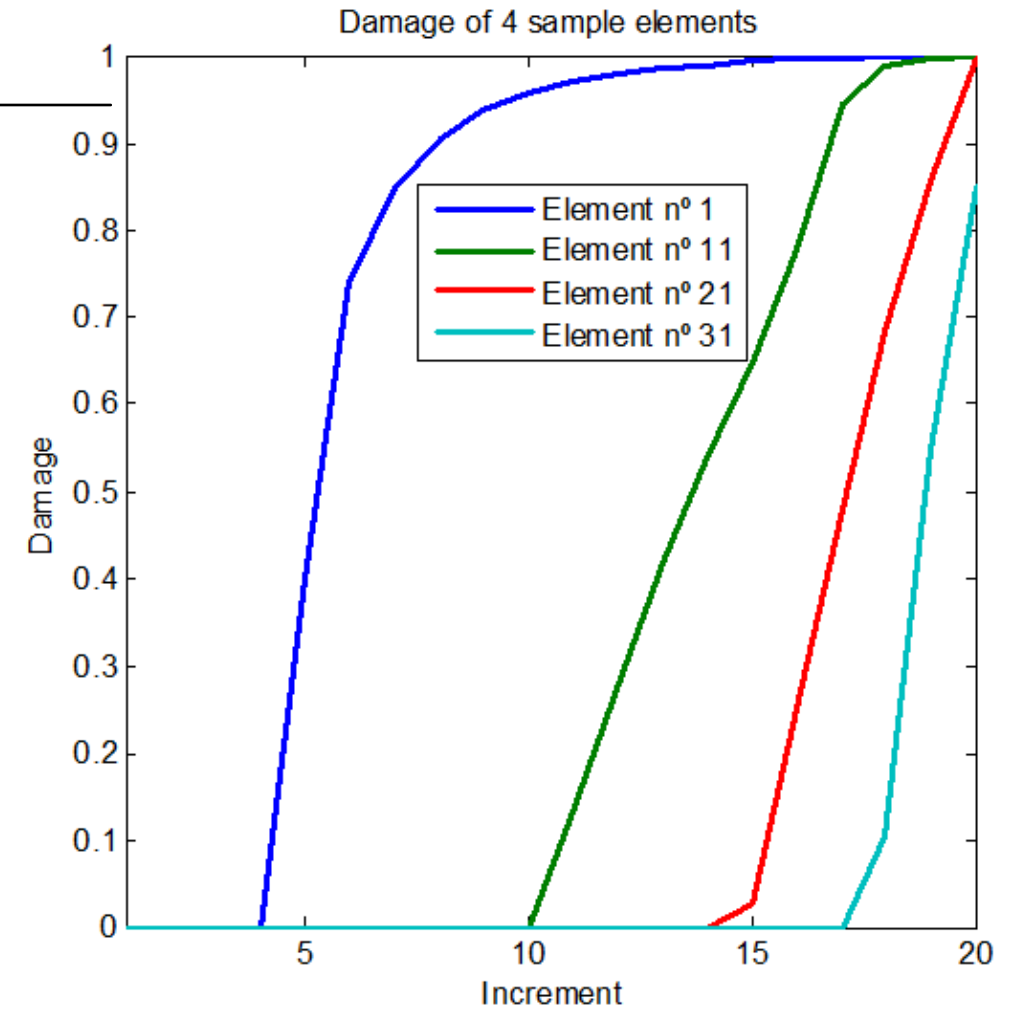
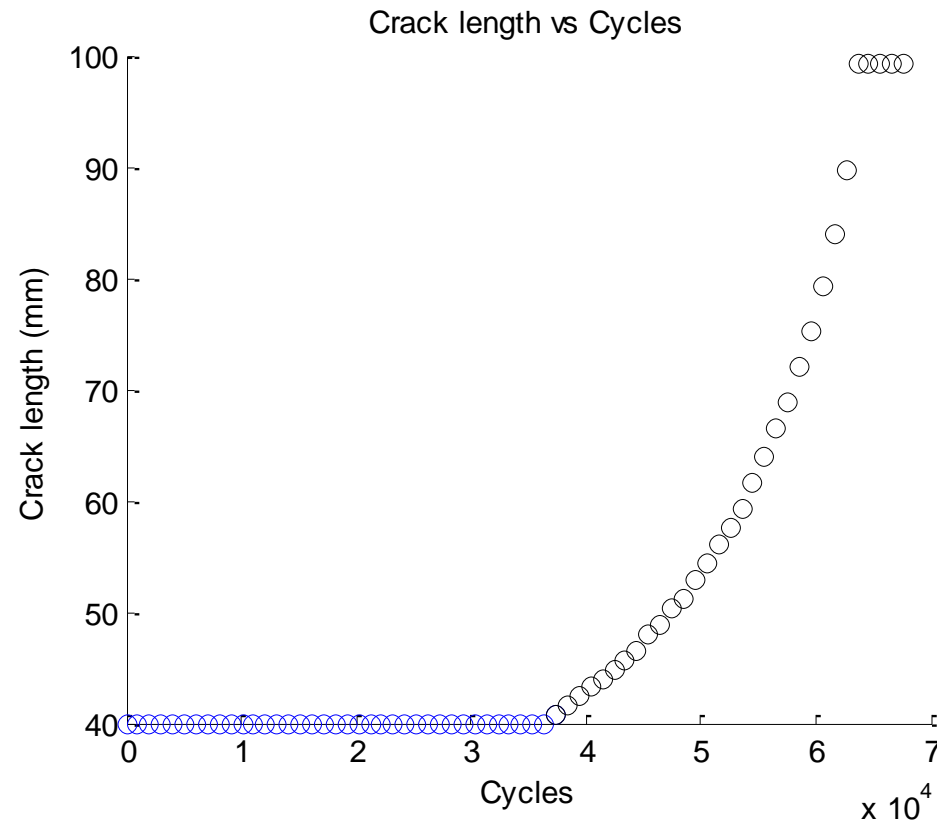
Fig. 8 – Resulting deformed configuration.

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Numerical modelling - methodology

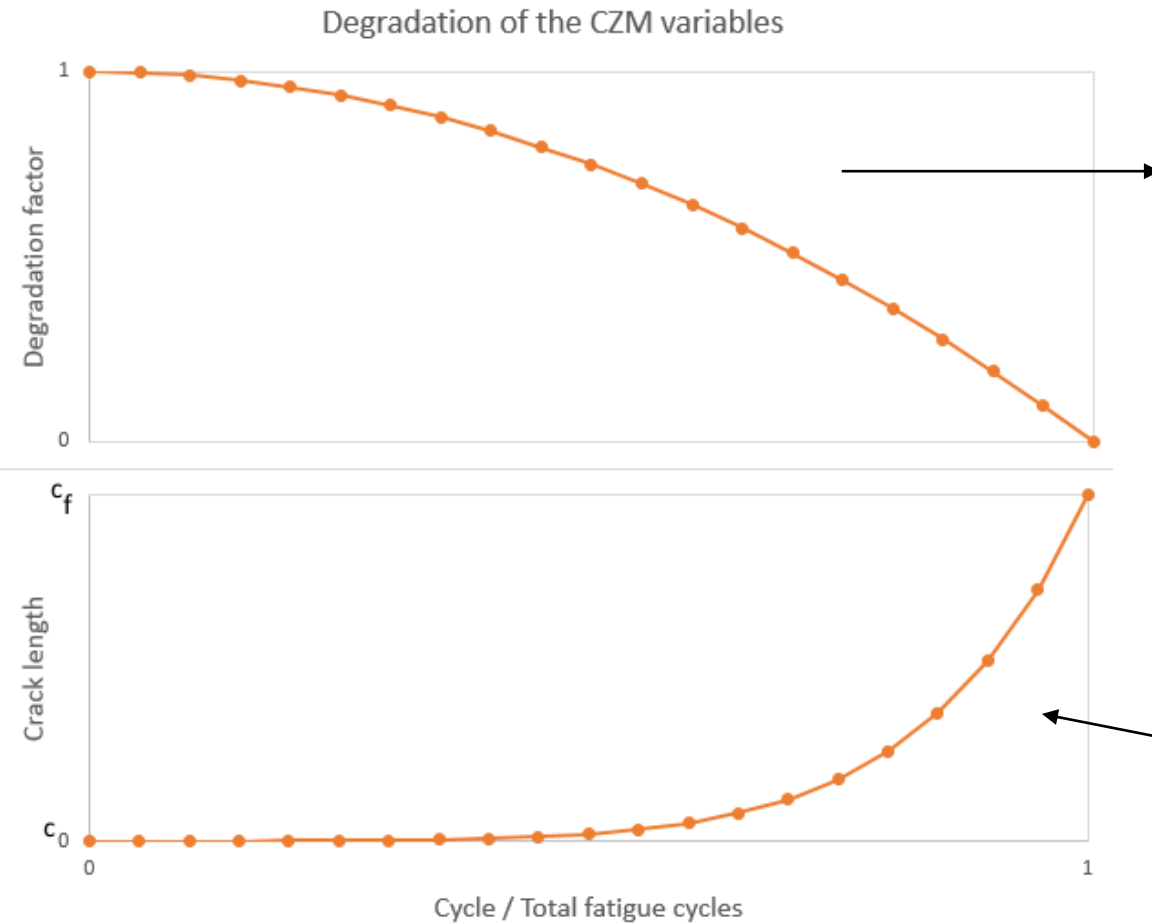
If totally damaged, crack length is calculated. If partially damaged, it belongs in the FPZ.



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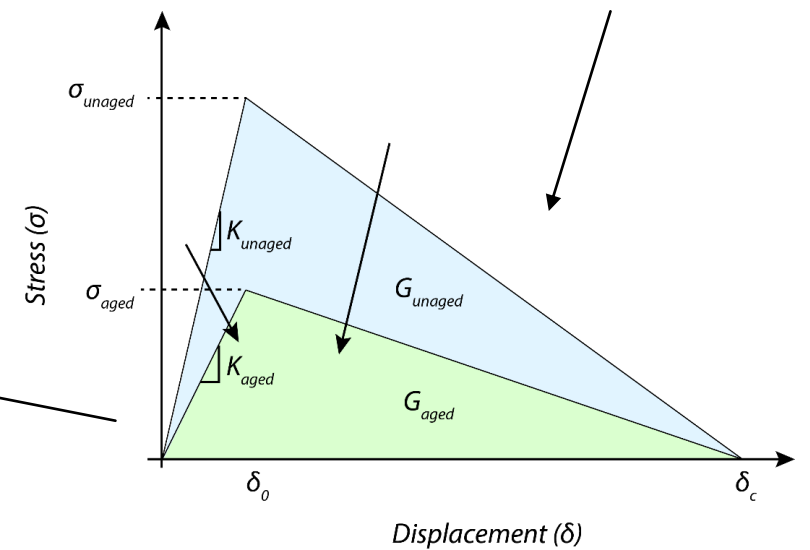
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Numerical modelling - degradation



$$\sigma_{aged} = \sigma_{unaged} \cdot \left(1 - \frac{\text{increment}}{\text{total increments}}\right)^2$$

$$G_{aged} = G_{unaged} \cdot \left(1 - \frac{\text{increment}}{\text{total increments}}\right)^2$$



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Conclusions

- **Experimental data for humidity is a slow process;**
- **UEL routine is behaving like expected;**
- **Humidity + Fatigue will provide a robust tool for predicting the future effects on the adhesive joints.**

Future work

- **More experimental testing is needed (humidity at various stages, fatigue with humid joints, etc.);**
- **Using those results to find the exact relationship between aged and unaged parameters;**
- **Implement the relationship in the UEL routine.**

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